Application of Control Principles to Co-Design

Tuhin K Das,

Associate Professor,

University of Central Florida,

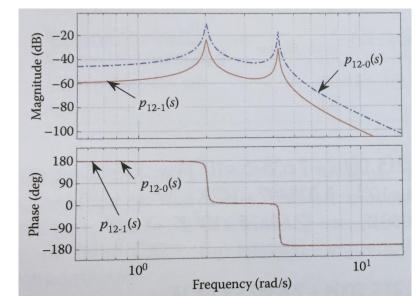
Orlando, FL 32816,

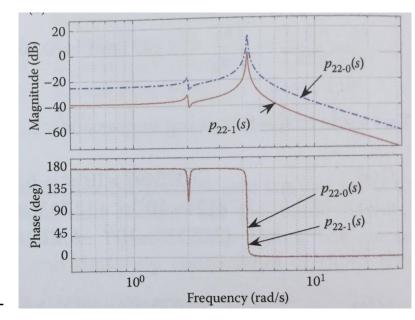
E-mail: Tuhin.Das@ucf.edu



Exploiting vibrational characteristics in control co-design

- Resonance frequencies: Operating frequencies where oscillation amplitudes sharply increase
 - Locations based on geometry, mass distribution, dynamic interconnections
 - Points of high cyclic stresses
 - Sharpness of peak and slope of phase plot provide estimate of the amount of damping
- In certain cases operating under resonance conditions must be avoided
 - e.g. wind turbine
 - Drive engineering design to appropriately place the resonance points, or
 - Design controllers to reduce bandwidth
- In other applications, resonant oscillation can be utilized to harvest energy
 - e.g. Resonant wave energy harvesting

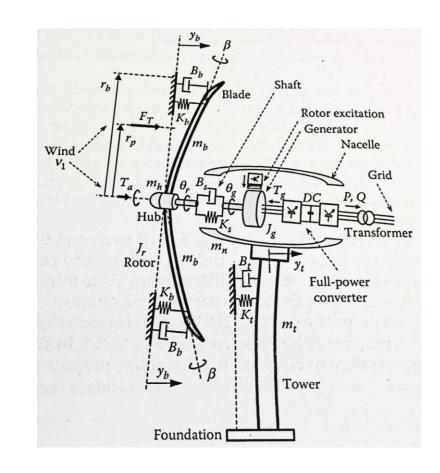




^{*} M. Garcia-Sanz, "Robust Control Engineering," CRC Press, 2017

Exploiting vibrational characteristics (Wind Turbines, Wave Energy)

- Under high wind speeds, blade pitch control is essential for capping the power output and for protecting mechanical components
 - Such high wind speeds could excite excessive vibrations in the structure (hence a need to <u>prevent resonance</u>)
 - Isolated blade pitch controllers may overlook this issue
 - Lumped parameter 3DOF vibration models, capture potential resonance situations enabling more practical control design*
 - The exercise shows how <u>dynamic vibration absorption</u> or <u>mechanical design iterations</u> (i.e. <u>control co-design</u>) could improve overall system characteristics.
- In wave energy converters, <u>resonance conditions are</u> desired to maximize energy harvesting**
 - The concept is utilized in resonant driven buoys whose natural frequency is tuned to match that of the waves.

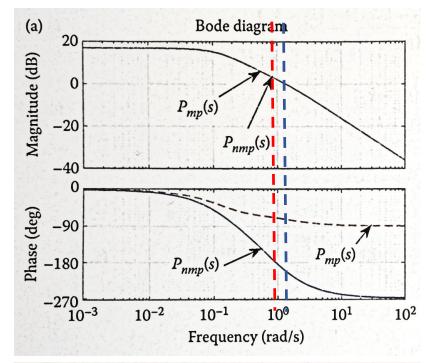


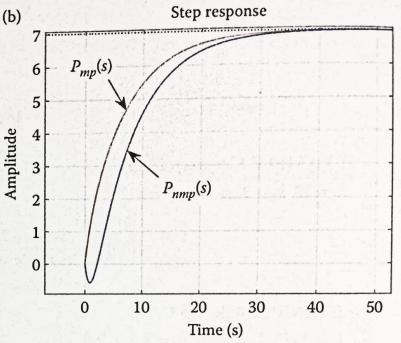
^{*} M. Garcia-Sanz, "Robust Control Engineering," CRC Press, 2017

^{**} D. A. Gemme, H. R. Greene II, T. A. Tucker, R. B. Sepe Jr., S. P. Bastien, "Hybrid Resonant Wave Energy Harvesting Buoy for Sensor Applications," 2013 OCEANS, San Diego

Nonminimum-Phase (NMP) Zero*, **

- An NMP zero poses constraints on robust stability
 - NMP zeros have positive real parts
 - An NMP zero reduces robustness by reducing Gain and Phase margins (GM and PM) (bandwidth limitations)
 - Characterized by an <u>initial inverse response</u> to step input
- Pole NMP-zero cancellation introduces or retains internal instability
- To address constraints due to NMP zeros:
 - Use <u>control strategies</u>, e.g. change input/output variable(s), use of feedforward action
 - Adopt co-design approach: Revisit system design and change sensing/actuation configurations or change dynamic characteristics





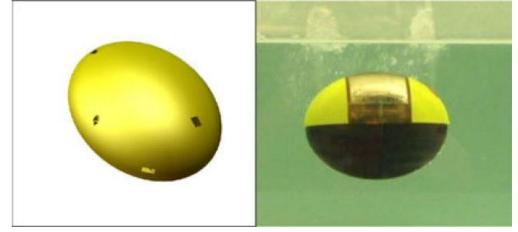
^{*} M. Garcia-Sanz, "Robust Control Engineering," CRC Press, 2017

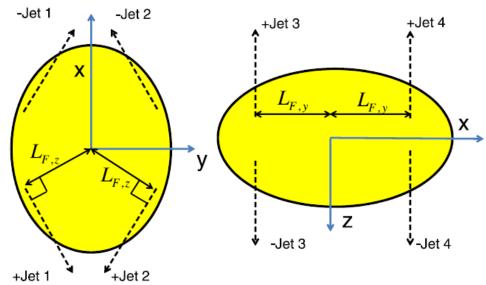
** J. B. Hoagg, D. S. Bernstein, "Nonminimum-Phase Zeros," IEEE Control

^{**} J. B. Hoagg, D. S. Bernstein, "Nonminimum-Phase Zeros," IEEE Control Systems Magazine, June 2007

Control-Configured Underwater Vehicle*

- A spheroidal underwater surveillance/ inspection robot with no appendages or fins for locomotion
 - Ability to turn in place, conduct precise inspection
 - Agile and causing minimum water perturbation
 - Minimum interference or collision during task
- The shape has inherent instabilities (e.g. Munk moment) but is well-suited for tasks
- Fixed-angle jets were designed for control
 - Jets were designed to <u>prevent NMP characteristics</u> and <u>uncontrollable modes</u>
 - Inward angled jets led to <u>unstable but easily</u> <u>stabilizable dynamics</u>
 - Actuations designed to <u>aid controllability</u>





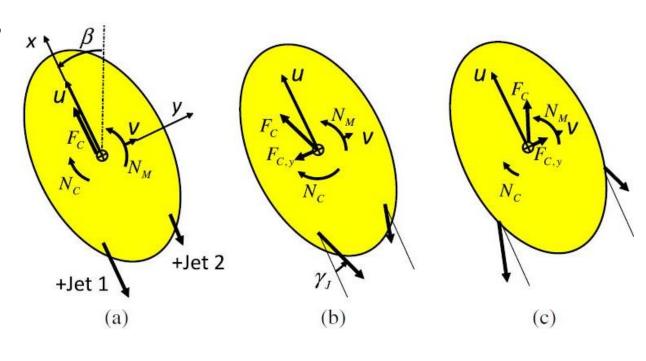
^{*} A. Mazumdar, H. H. Asada, "Control-Configured Design of Spheroidal, Appendage-Free, Underwater Vehicles," IEEE Trans. Robotics, Vol. 30, No. 2, April 2014

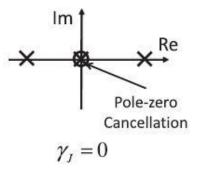
Control-Configured Underwater Vehicle*

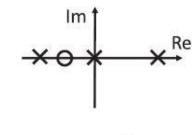
Transfer function of linearized dynamics

$$\frac{\Delta \psi(s)}{\Delta V(s)} = \frac{\left(sG_M m_y + \Delta m_a U_c G_F \sin \gamma_J\right)}{s\left(m_y I_z s^2 - U_c^2 m \Delta m_a\right)}$$

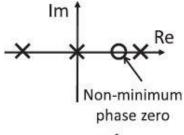
- Parallel jets: Pole-zero cancellation
 - No control on side-slip
 - Loss of controllability
- Inward jets:
 - Both side-slip and Munk moment opposed
 - Zero in LHP
- Outward jets:
 - Cancelling one tends to amplify the other
 - NMP zero
- Note: Unstable in all cases











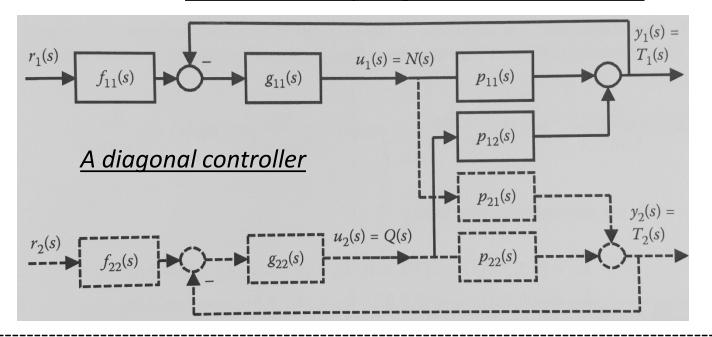
$$\gamma_J = -30^\circ$$
(c)

(C

^{*} A. Mazumdar, H. H. Asada, "Control-Configured Design of Spheroidal, Appendage-Free, Underwater Vehicles," IEEE Trans. Robotics, Vol. 30, No. 2, April 2014

MIMO systems: Heat exchanger control*

- MIMO systems are <u>dynamically coupled</u>
 - Transfer function is a matrix instead of scalar
 - Typical control methods involve <u>pairing</u> of specific input variables to specific output variables
 - The pairing can be based on <u>Relative Gain Array</u> (RGA) analysis and/or <u>analysis of the dynamic equations</u>
 - However, the inherent coupling that will still exist

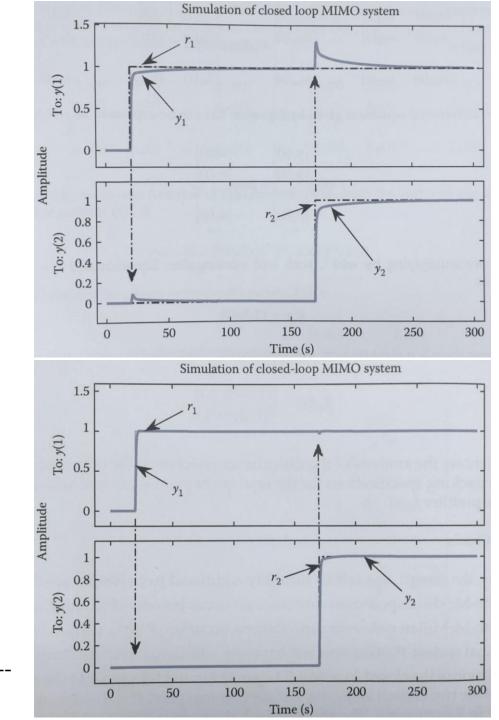


Hot fluid tank Hot Heat water exchanger Product Constant flow $T_1(s)$ N(s) $p_{11}(s)$ $p_{12}(s)$ Q(s)

* M. Garcia-Sanz, "Robust Control Engineering," CRC Press, 2017

MIMO: Heat exchanger control*

- Internal coupling persists in pairing based control
 - Set point changes in references cause <u>perturbation</u> in the coupled variables
 - Desire a performance to achieve the result shown below – <u>a significantly better decoupling of</u> <u>dynamics</u>
- Approaches to achieve this:
 - Through control design
 - E.g. feedback based decoupling, redefining control inputs
 - Through control co-design
 - Revisiting and modifying system design
 - E.g. introducing alternate flow paths (actuations)
 - Also exploring if there is any fundamental obstacle to decoupling



^{*} M. Garcia-Sanz, "Robust Control Engineering," CRC Press, 2017